Segment-Weighted Information-Based Event-Triggered Mechanism for Networked Control Systems

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Abstract-In this study, the event-triggered problem of networked control systems (NCSs) is investigated, and a novel information transmission scheme is established. Under this scheme, the segment-weighted information (SWI) in a sliding historical window (SHW) is calculated and then sampled. Compared with the traditional direct sampling method, in this approach, the control input includes historical information in the SHW, thereby leading to less information loss due to sampling. This study also emphasizes on designing an SWI-based event-triggered mechanism (ETM) for scheduling network transmission. Different from most of the existing ETMs, the proposed SWI-based ETM leverages historical information to determine which data are necessary for the whole control system. Our approach can greatly reduce the number of unexpected triggering events of a control system with stochastic disturbances owing to the introduction of the SWI in the ETM. Moreover, Zeno phenomena are prevented thanks to periodic sampling. Sufficient conditions are derived based on the Lyapunov functional approach, and a numerical simulation example is provided to demonstrate the effectiveness of the proposed method.

Index Terms—Event-triggered mechanism (ETM), networked control system (NCS), segment-weighted information (SWI), sliding historical window (SHW).

I. INTRODUCTION

O WING to the rapid development and ever-increasing application of communication technologies, more and more control systems are being equipped with a network

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for signal transmission. During the last two decades, networked control systems (NCSs) have attracted growing interest [1], [2], [3], [4]; the information is shared among the sensors, controllers, and actuators through a communication network. Owing to the limited network bandwidth, engineers encounter certain challenges when modeling and analyzing NCSs; some examples are network congestion [5], [6], [7], [8], networked-induced delay, packet dropout and disordering during transmission [9], [10], and constraints regarding the energy, communication, and computational resources.

Sampling and release are essential actions of NCSs. Reseaches have extensively investigated sampled-data control for continuous-time systems with sampled-data outputs. In general, there are two relatively mature sampled-data control methods. The first method is the periodic sampling scheme. Most of the published research results and applications are based on this scheme. The focus of these studies was to determine approaches that ensure stability and stabilize a system with a lower level of conservatism. For example, in [11], the stability of sampled-data control systems with uncertainty is assessed with a Lyapunov-Krasovskii functional method. The researches in [12] constructed time-dependent Lyapunov functionals to obtain the upper bound of the sampling period. To establish a time-dependent Lyapunov functional method with a lower level of conservatism, the researches in [13] created a stabilization approach based on Wirtinger's inequality. In this time-triggered mechanism (TTM), the worst situation in which the system works is usually considered for the selection of a fixed sampling period. Therefore, hardware costs and the consumption of communication and computational resources increase inevitably. Consequently, the second type of sampling scheme (i.e., aperiodic sampling) has gained much attention. The main problem of this scheme is estimating the maximum sampling interval to ensure that the system remains stable [14]. Transforming a system into a time-delay system [15], hybrid system [16], and discrete-time system [17] is a popular way to analyze a system with an aperiodic sampling scheme.

As previously mentioned, periodic sampling and release may result in the waste of network and computational resources. The study of the event-triggered mechanism (ETM) has become a hot topic to alleviate the network burden. In the ETM, the choice to release or sample depends on an eventtriggered condition instead of a predetermined fixed period.

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The ETM determines the next sampling instant and the next release instant. For example, Girard [18] and Ge et al. [19] created a dynamic ETM by introducing dynamic variables to determine the next sampling instant. These types of ETMs essentially involve the aperiodic sampling scheme. The Zeno phenomenon is a challenging issue that should be considered in the study of ETM design. To solve this problem, discrete event-triggered strategies (DETSs) [20], [21], [22] for linear networked systems were investigated to decrease the data transmission rate and save network bandwidth. Wen et al. [23] combined the DETS and sliding-mode control method to design a control strategy for nonlinear systems. The DETS uses a TTM for sampling and an ETM for release; the Zeno phenomenon can be easily excluded by physical means. Extended DETSs are widely applied in NCSs. For example, the threshold of the ETM in [7] was designed as an adaptive variable; hence, the data-release rate is adjusted with the state variation. Hu et al. [24] and Gu et al. [25] developed a resilient event-triggered transmission protocol that addresses denial of service (DoS) attacks. In [26], similar transmission scheme was developed for semi-Markovian switching cyberphysical systems. Based on the past transmitted information, a class of memory-based ETMs was investigated in [27] and [28]. However, under this type of ETM, only a few discrete packets can be used to improve the triggering mechanism. Selivanov and Fridman [29] investigated a trade-off eventtriggered method between a DETS and continuous ETM by using a switched system approach, under which the ETM is executed after a fixed waiting time to prevent the Zeno phenomenon. Although this method uses a continuous-time state as the ETM input, a waiting period is needed to prevent the Zeno phenomena. A controller with general sampling methods loses vital information of the plant during the fixed sampling period; however, few researches have focused on this problem; therefore, it is one of the main motivations of this study.

Historical information is essential for both the controller and ETM to ensure a good control performance and data-release rate [30], [31]. In practical systems using traditional ETMs, information at a certain instant may trigger unexpected packets. Thus, the burden on the network bandwidth increases, in particular, when the system is subject to random disturbances. A continuous-type ETM (e.g., integral-type ETM) can introduce historical information into the system [32], [33]. However, it is difficult to ensure the interevent time. In addition, a system with a memory-based control strategy can achieve a better control performance than one with a memory-less control strategy. However, few researches have considered these challenging problems of event-triggered control systems.

This study focuses on the design of a new SWI-based eventtriggered control strategy for NCSs. The main contributions of this study are highlighted as follows.

 A novel event-triggered control strategy for NCSs that combines the advantages of the DETS and continuous ETM is presented. Unlike in the conventional periodically sampled event-triggered system, an SWI module is introduced before sampling. The input of the designed ETM uses the segment-weighted information (SWI) in a sliding historical window (SHW) to determine the next



Fig. 1. Framework of SWI-based event-triggered control method.

event-triggering instant. It can significantly reduce the amount of unexpected released data compared to the already existing communication mechanisms, in particular, for a system with uncertain stochastic disturbances.

2) The SWI in an SHW is split into N segments. The closer information to the current instant, the greater the weight of the SWI is. Our approach has a better control performance than traditional memoryless control strategies because the control input introduces sampled SWI with historical information.

Notation: Let $\mathbf{He}(X) := X^T + X$ and $\mathbf{Sy}(M, N) := N^T M N$; I_r is the $r \times r$ identity matrix and $\mathbb{I}_j := [\underbrace{0, \dots, 0}_{j-1}, I, 0, \dots, 0].$

II. PRELIMINARIES AND PROBLEM FORMULATION

The physical system is described by the following continuous-time linear system:

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) + Ed(t) \\ z(t) = Cx(t) \end{cases}$$
(1)

where *A*, *B*, *C*, and *E* are known real matrices of appropriate dimensions, $x(t) \in \mathbb{R}^n$ is the state vector; $u(t) \in \mathbb{R}^m$ is the control input; $z(t) \in \mathbb{R}^r$ is the output; and d(t) is an exogenous disturbance belonging to $\mathscr{L}_2[0, \infty)$.

To exploit the historical information in the control loop, a new variable with SWI from t - w to t is introduced

$$\bar{x}(t) = \sum_{p=1}^{N} \frac{\mu_p}{\bar{w}} \int_{t-w_p}^{t-w_{p-1}} x(s) ds$$
(2)

with $w_0 = 0$, $w_N = w$, where $\sum_{p=1}^{N} \mu_p = 1$ and $\bigcup_{i=1}^{N} [t - w_{p-1}, t - w_p) = [t - w, t]$; t - w to t represents the SHW.

For a convenient design, setting $w_p - w_{p-1} = \bar{w}$ yields $w_p = p\bar{w}$, where \bar{w} is a known constant.

As is shown in Fig. 1, the SWI is sampled periodically with the sampling period *h* and transmitted over the network at instant t_kh only when it satisfies the prescribed triggering condition where $0 < t_0 < t_1 \cdots < t_k \cdots$. The zero-order hold (ZOH) is needed before the signal from the network enters

the controller. Subsequently, a quasi-state feedback control strategy is constructed

$$u(t) = K\bar{x}(t_k h) \tag{3}$$

for $t \in [t_k, t_{k+1})$.

Remark 1: Unlike the memoryless state feedback control law, the control input in (3) is a memory control strategy that depends on a new state that includes historical information in the SHW. Furthermore, the controller in the traditional direct sampling method loses all information between the adjacent sampling instants. Historical information is leveraged under the proposed SWI-based control strategy, which improves the control performance.

Remark 2: If N packets with SWIs are packed one to transmit over the network, the memory-based control law can be constructed as follows:

$$u(t) = \sum_{p=1}^{N} K_p \frac{\mu_p}{\bar{w}} \int_{t-w_p}^{t-w_{p-1}} x(s) ds$$
(4)

which improves the control performance. For simplicity, we assume that $K_i = K_i = K$ (i, j = 1, ..., N). Thus, (4) degrades to (3).

Define $\varepsilon(t) = \bar{x}(i_k h) - \bar{x}(t_k h)$, where $i_k h = t_k h + \ell h$ is a sampling instant with $\ell = 0, 1, 2, \dots, \ell$ in $[t_k, t_{k+1})$.

By borrowing the idea of traditional ETMs, we develop the following new SWI-based ETM:

$$\psi(t) = \varepsilon^{T}(t)\Lambda\varepsilon(t) - \theta\bar{x}^{T}(i_{k}h)\Lambda\bar{x}(i_{k}h) \ge 0.$$
(5)

After the module of SWI-based ETM, we know that the next data-transmission event will be triggered at instant $t_{k+1}h$, which is determined by

$$t_{k+1}h = t_kh + \min_{\ell > 0} \{\ell h | \psi(t) \ge 0\}.$$
 (6)

Remark 3: The use of historical information with forgetting factors as the input in the ETM in (5) can reduce the number of triggering events within a given time interval, in particular, when the system has uncertain random disturbances; only a few researches have studied this problem.

Remark 4: To apply reasonably historical information for the controller and ETM, μ_p is chosen such that it satisfies $\mu_1 > \mu_2 > \cdots > \mu_N$. Therefore, we call μ_p a forgetting factor; that is, the closer it is to the current time, the greater the weight of the state is. If we choose $\mu_i = \bar{w}/N$ (i = 1, ..., N), it degenerates into the idea in [34].

Remark 5: In addition to the advantages presented in Remarks 1 and 3, the scheme for calculating the SWI and then implementing periodic sampling (Fig. 1) can prevent the Zeno phenomena.

Remark 6: If we set N = 1 and $\bar{w} \rightarrow 0$, (3) and (6) become the traditional state feedback control method and ETM, respectively.

Remark 7: As depicted in Fig. 1, the SWI is designed before the sampler. Hence, the control strategy becomes a memory control approach. This new control structure can be applied to the NCS and sampling control system, which have a wide range of applications, such as the control of oxygen and carbon dioxide contents in blood [35].

For $l = 0, 1, \dots, \overline{l} - 1$, we define $\Omega_l \triangleq [t_k h + lh + d_l, t_k h + d_l]$ $(l+1)h + d_{l+1}$ with $d_0 = \eta_k$ and $d_{\bar{l}} = \eta_{k+1}$, where η_k is a network-induced delay at instant $t_k h$. Thus, $\Omega \triangleq [t_k h +$ $\eta_k, t_{k+1}h + \eta_{k+1}) = \bigcup_{l=0}^{l-1} \Omega_l.$

Owing to the use of the ZOH, from (2), we have

$$\bar{x}(t) = \bar{x}(i_k h) = \sum_{p=1}^{N} \frac{\mu_p}{\bar{w}} \int_{t_k h + lh - w_p}^{t_k h + lh - w_{p-1}} x(s) ds$$
(7)

for $t \in \Omega_l$.

Defining $\eta(t) = t - (t_k h + lh)$ for $t \in \Omega_l$ results the following relationship:

$$\bar{x}(t) = \bar{x}(i_k h) = \sum_{p=1}^{N} \frac{\mu_p}{\bar{w}} \int_{t-\eta(t)-w_p}^{t-\eta(t)-w_{p-1}} x(s) ds.$$
(8)

According to the definition of $\eta(t)$ and Ω_l , one knows that $0 \leq \eta(t) \leq h + \bar{d}_l \triangleq \eta_M.$

We define a new time-varying variable $d_p(t) \triangleq \eta(t) + w_p$ for $t \in \Omega_l$, evidently, $p\bar{w} \leq d_p(t) \leq \eta_M + p\bar{w} \triangleq d_{pM}$. Thus, (8) can be converted into

$$\bar{x}(i_k h) = \frac{1}{\bar{w}} \sum_{p=1}^{N} \mu_p \int_{t-d_p(t)}^{t-\eta(t)-(p-1)\bar{w}} x(s) ds.$$
(9)

Thus, it is true that

$$\bar{x}(i_k h) = \frac{1}{\bar{w}} \sum_{p=1}^{N} \mu_p \left[\int_{t-p\bar{w}}^{t-(p-1)\bar{w}} x(s) ds + \int_{t-d_p(t)}^{t-p\bar{w}} x(s) ds - \int_{t-d_{p-1}(t)}^{t-(p-1)\bar{w}} x(s) ds \right].$$
(10)

Before formulating the closed-loop system, we introduce the definition of Legendre polynomials

$$L_{i}(s) = (-1)^{i} \sum_{\nu=0}^{i} G_{\nu}^{i} \left(\frac{s-a}{b-a}\right)^{i}, \ G_{\nu}^{i} = (-1)^{i} \binom{i}{\nu} \binom{i+\nu}{i} (11)$$

and their properties.

1) For $\forall \nu \in \mathbb{N}$, $(b - a) \int_a^b \mathcal{L}_{\nu}^T(s) \mathcal{L}_{\nu}(s) ds = W_{\nu}$, where $\mathcal{L}_{\nu}(s) \triangleq [L_0(s) \cdots L_i(s) \cdots L_{\nu}(s)]^T$ and $W_{\nu} =$ diag{1, 3, ..., $2\nu + 1$ }. 2) $\dot{L}(s) = \begin{cases} 0, & i = 0\\ \sum_{k=0}^{i-1} \frac{(2i+1)}{2}(1-(-1)^{i+k}), & i > 1 \end{cases}$.

$$\sum_{k=0}^{\infty} \frac{\sum_{k=0}^{\infty} (1 - (-1)^{i+k}), i \ge 1}{b-a}$$

3) For $\forall i \in \mathbb{N}, L_i(a) = (-1)^i, L_i(b) = 1.$

Remark 8: In this study, we apply the above properties of Legendre polynomials to replace the method in which the approximate average measurement output in [34] is applied, thereby making the proof more solid, which has been a big challenge of this study.

By combining (1) and (10), we obtain the following closedloop control system for $t \in \Omega_l$:

$$\dot{x}(t) = Ax(t) + BK \sum_{p=1}^{N} \frac{\mu_p}{\bar{w}} \int_{t-p\bar{w}}^{t-(p-1)\bar{w}} x(s) ds + BK \sum_{p=1}^{N} \frac{\mu_p}{\bar{w}} \int_{t-d_p(t)}^{t-p\bar{w}} x(s) ds$$

$$-BK \sum_{p=1}^{N} \frac{\mu_{p}}{\bar{w}} \int_{t-d_{p-1}(t)}^{t-(p-1)\bar{w}} x(s) ds -BK\varepsilon(t) + Ed(t) = Ax(t) - BK\varepsilon(t) + Ed(t) + BK \sum_{p=1}^{N} \frac{\mu_{p}}{\bar{w}} \Big[-\Omega_{1,1}^{p}(t) + \Omega_{2}^{p}(t) + \Omega_{3,1}^{p}(t) \Big]$$
(12)

where

$$\Omega_{1,1}^{p}(t) = \int_{-d_{p-1}(t)}^{-(p-1)\bar{w}} \mathbb{L}^{1}(s)x(t+s)ds$$
$$\Omega_{2}^{p}(t) = \int_{-p\bar{w}}^{-(p-1)\bar{w}} \mathbb{L}^{2}(s)x(t+s)ds$$
$$\Omega_{3,1}^{p}(t) = \int_{-d_{p}(t)}^{-p\bar{w}} \mathbb{L}^{3}(s)x(t+s)ds.$$

In this study, we develop a memory-based state feedback control strategy for system (1) with the proposed SWI-based ETM. The block diagram is depicted in Fig. 1.

III. MAIN RESULTS

The following lemma is useful for the subsequent results. *Lemma 1:* For matrices $R \in \mathbb{R}^{q \times q} > 0$, $Y \in \mathbb{R}^{q \times q}$, and $\mathcal{R} = \begin{bmatrix} R & Y \\ Y^T & R \end{bmatrix} > 0$ and the vector function $x : [a, b] \to \mathbb{R}^{q}$, we have

$$\int_{a}^{b} \mathbf{Sy}(R, x(s)) ds \geq \frac{1}{b-a} \mathbf{Sy} \left(\mathcal{R} \otimes W_{\nu}, \begin{bmatrix} \mathbb{K}_{q,\nu} & 0_{\nu q} \\ 0_{\nu q} & \mathbb{K}_{q,\nu} \end{bmatrix} \Omega_{\nu} \right)$$
(13)

where $\Omega_{\nu} = \begin{bmatrix} \int_{c}^{b} \mathbb{L}_{\nu}(s)x(s)ds \\ \int_{a}^{c} \mathbb{L}_{\nu}(s)x(s)ds \end{bmatrix}$, $\mathbb{L}_{\nu}(s) \triangleq \mathcal{L}_{\nu}(s) \otimes I_{q}, c \in [a, b]$, and $W_{\nu} = \operatorname{diag}\{1, 3, \dots, 2\nu + 1\}$.

Proof: Let $\mathbf{f}(s) = \mathcal{L}_{\nu}(s)$ and $\varpi(s) = 1$ for [4, Lemma 3]; The proof is complete.

Remark 9: In (13), the matrix $\mathbb{K}_{q,\nu} \in \mathbb{R}^{q\nu \times q\nu}$ can be obtained by using the MATLAB instruction **vecperm** (q, ν) presented in [36]. It has the same property as that in [4, Lemma 2].

Theorem 1: For the scalars \bar{w} , α , θ , controller gain K, and prespecified H_{∞} attenuation level γ , the system (12) is asymptotically stable if there exist symmetric matrices P, $R_{1p} > 0$, $R_{2p} > 0$, $R_{3p} > 0$, $Q_{1p} > 0$, $Q_{2p} > 0$, $Q_{3p} > 0$, $\Lambda > 0$, $Q_{1(p-1)} > 0$, and $Q_{3p} > 0$ with $p = 1, \ldots, N$, and a matrix G such that

$$\mathscr{P} > 0 \text{ and } \Theta < 0$$
 (14)

where

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$$\mathcal{P} = P + \operatorname{diag}\{0, \mathfrak{Q}_1, \mathfrak{Q}_2, \mathfrak{Q}_3\}$$
$$\Theta = \operatorname{He}(\mathcal{M}^T P \mathcal{H})$$
$$+ \sum_{p=1}^{N} \left[\operatorname{Sy}(\hat{\mathcal{T}}_{2p}, \mathbb{I}_{1+p}) - \operatorname{Sy}(R_{1p}, \mathbb{I}_{2+p+N}) \right]$$
$$- \operatorname{Sy}(W_{\nu} \otimes \mathfrak{Q}_1, \mathbf{K} \mathbb{I}_{1,N})$$

$$\begin{split} &+ \sum_{p=1}^{N} \left[\operatorname{Sy}(\hat{T}_{3p}, \mathbb{I}_{1+p}) - \operatorname{Sy}(R_{2p}, \mathbb{I}_{2+p}) \right] \\ &+ \sum_{p=1}^{N} \left[\operatorname{Sy}(\hat{T}_{4p}, \mathbb{I}_{2+p}) - \operatorname{Sy}(R_{3p}, \mathbb{I}_{3+p+N}) \right] \\ &- \operatorname{Sy}(W_{v} \otimes \mathfrak{Q}_{2}, \mathbb{I}_{2,N}) - \operatorname{Sy}(W_{v} \otimes \mathfrak{Q}_{3}, \mathbb{KI}_{3,N}) \\ &+ \operatorname{Sy}\left(\left[\begin{bmatrix} -\Lambda & 0 \\ 0 & -\theta \Delta \right] \right] \cdot \left[\begin{bmatrix} \mathbb{I}_{3} \\ \mathbb{I}_{3} \end{bmatrix} \right] - \gamma^{2} \operatorname{Sy}(I_{q}, \mathbb{I}_{d}) \\ &- \operatorname{Sy}(I_{q}, \mathbb{I}_{2}) + \operatorname{He}(\mathbb{I}_{c}^{T} \mathbb{C}\mathbb{I}_{2}) + \operatorname{He}(\mathcal{G}\mathcal{F}) \\ &\mathfrak{Q}_{1} = \operatorname{diag}\left\{ \frac{1}{\eta_{M}} \mathcal{Q}_{10}, \dots, \frac{1}{\eta_{M}} \mathcal{Q}_{2p}, \dots, \frac{1}{\eta_{M}} \mathcal{Q}_{1(p-1)} \right\} \\ &\mathfrak{Q}_{2} = \operatorname{diag}\left\{ \frac{1}{\eta_{M}} \mathcal{Q}_{21}, \dots, \frac{1}{\eta_{M}} \mathcal{Q}_{2p}, \dots, \frac{1}{\eta_{M}} \mathcal{Q}_{3N} \right\} \\ &\mathfrak{Q}_{1(p-1)} = \begin{bmatrix} \mathcal{Q}_{1p} & * \\ \mathcal{H}_{1p} & \mathcal{Q}_{1p} \end{bmatrix}, \quad \mathcal{Q}_{2p} = \mathcal{Q}_{2p}, \quad \mathcal{Q}_{3p} = \begin{bmatrix} \mathcal{Q}_{3p} & * \\ \mathcal{H}_{3p} & \mathcal{Q}_{3p} \end{bmatrix} \\ &\mathbf{K} = \operatorname{diag}(\mathbb{K}, \dots, \mathbb{K}), \quad \mathbb{K} = \begin{bmatrix} \mathbb{K}_{n, \nu+1} & 0(\nu+1)n \\ 0(\nu+1)n & \mathbb{K}_{n, \nu+1} \end{bmatrix} \\ &\mathbb{I}_{\overline{X}} = \sum_{p=1}^{N} \frac{\mu_{p}}{W} \begin{bmatrix} \mathbb{I}_{3+2N+2N(\nu+1)+p} - \mathbb{I}_{m(p,\nu,1,1)} + \mathbb{I}_{m(p,\nu,3,1)} \end{bmatrix} \\ &m(p, \nu, j, k) = 3 + 2N + 1.5(j - 1)N(\nu + 1) \\ &+ 2(p - 1)(\nu + 1) + k, j = 1, 3 \\ &\hat{7}_{2p} = R_{1p} + \eta_{M} \mathcal{Q}_{2p}, \quad \mathbb{I}_{d} = \mathbb{I}_{3+2N+5N(\nu+1)+1} \\ &\hat{7}_{\overline{3}p} = R_{2p} + \bar{w} \mathcal{Q}_{2p}, \quad \mathbb{I}_{d} = \mathbb{I}_{3+2N+5N(\nu+1)+2} \\ &\hat{7}_{ap} = R_{3p} + \eta_{M} \mathcal{Q}_{3p}, \quad \mathbb{I}_{z} = \mathbb{I}_{3+2N+5N(\nu+1)+2} \\ &\hat{7}_{ap} = R_{3p} + \eta_{M} \mathcal{Q}_{3p}, \quad \mathbb{I}_{z} = \mathbb{I}_{3+2N+5N(\nu+1)+3} \\ &\mathcal{F} = -\mathbb{I}_{1} + A\mathbb{I}_{2} - BK\mathbb{I}_{e} + E\mathbb{I}_{d} \\ &+ BK \sum_{p=1}^{N} \frac{\mu_{p}}{\mu_{p}} \left[\mathbb{I}_{p}^{T} + \mathbb{I}_{3,1}^{T} - \mathbb{I}_{1,1}^{T} \right] \\ &\mathbb{I}_{1,1}^{T} = \mathbb{I}_{1,1}^{T} \cdots \mathcal{I}_{3,N}^{T} \\ &\mathcal{J}_{1,1}^{T} = \mathbb{I}_{1,1}^{T} \cdots \mathcal{J}_{3,N}^{T} \\ &\mathcal{J}_{1,1}^{T} = \mathbb{I}_{1,1}^{T} \cdots \mathcal{J}_{3,N}^{T} \\ &\mathcal{J}_{1,1}^{T} = \mathbb{I}_{1,2}^{T} \cdots \mathcal{J}_{3,N}^{T} \\ &\mathcal{J}_{1,2}^{T} = \mathbb{I}_{1,1}^{T} \cdots \mathcal{J}_{2,N}^{T} \\ \\ &\mathbb{I}_{1,N}^{T} = \mathbb{I}_{1,N}^{T} \cdots \mathcal{J}_{1,N}^{T} \\ &\mathbb{I}_{2,N}^{T} = \mathbb{I}_{1,N}^{T} \cdots \mathbb{I}_{3,N}^{T} \\ &\mathbb{I}_{1,N}^{T} = \mathbb{I}_{1,N}^{T} \cdots \mathbb{I}_{3,N}^{T} \\ \\ &\mathbb{I}_{1,N}^{T} = \mathbb{I}_{1,N}^{T} \cdots \mathbb{I}_{3,N}^{T} \\ \\ &\mathbb{I}_{1,N}^{T} = \mathbb{I}_{1,N}^{T} \cdots \mathbb{I}_{3,N}^{T} \\ \\$$

$$\begin{split} \mathbb{E}_{1,N}^{p} \stackrel{T}{=} \begin{bmatrix} \mathbb{E}_{1,N}^{p,1} \stackrel{T}{\mathbb{E}_{1,N}} \end{bmatrix}, & \mathbb{E}_{3,N}^{p} \stackrel{T}{=} \begin{bmatrix} \mathbb{E}_{3,N}^{p,1} \stackrel{T}{\mathbb{E}_{3,N}} \end{bmatrix} \\ \mathbb{E}_{j,N}^{p,1} = \begin{bmatrix} \mathbb{I}_{m(p,\nu,j,1)} \\ \vdots \\ \mathbb{I}_{m(p,\nu,j,(\nu+1))} \end{bmatrix}, & \mathbb{E}_{j,N}^{p,2} = \begin{bmatrix} \mathbb{I}_{m(p,\nu,j,(\nu+2))} \\ \vdots \\ \mathbb{I}_{m(p,\nu,j,2(\nu+1))} \end{bmatrix} \\ \mathbb{E}_{2,N}^{p} = \begin{bmatrix} \mathbb{I}_{3+2N+2N(\nu+1)+(p-1)(\nu+1)+1} \\ \vdots \\ \mathbb{I}_{3+2N+2N(\nu+1)+p(\nu+1)} \end{bmatrix} \\ \Pi_{\nu} = \begin{bmatrix} \pi_{0}^{0}I & \cdots & \pi_{0}^{\nu}I \\ \vdots & \pi_{g}^{i} & \vdots \\ \pi_{\nu}^{0}I & \cdots & \pi_{\nu}^{\nu}I \end{bmatrix} \\ \pi_{g}^{i} = \begin{cases} -(2i+1)(1-(-1)^{g+i}), & i \leq g \\ 0, & i > g. \end{cases} \end{split}$$

Proof: For simplicity, we define

$$\boldsymbol{\zeta}(t) = \left[\boldsymbol{x}^T(t), \mathcal{L}^{1T}(t), \mathcal{L}^{2T}(t), \mathcal{L}^{3T}(t) \right]^T$$

with $\mathscr{L}^{1}(t) = [\int_{-d_{0M}}^{0} \mathfrak{L}_{1}^{T}(s,t)dv, \dots \int_{-d_{(p-1)M}}^{-(p-1)\bar{w}} \mathscr{L}_{1}^{T}(s,t)ds$ $,\dots, \int_{-d_{(N-1)M}}^{-(N-1)\bar{w}} \mathscr{L}_{1}^{T}(s,t)ds]^{T}, \quad \mathscr{L}^{2}(t) = [\Omega_{2}^{1T}(t),\dots, \Omega_{2}^{pT}(t),\dots, \Omega_{2}^{pT}(t)], \quad \mathscr{L}^{3}(t) = [\int_{-d_{1M}}^{-\bar{w}} \mathscr{L}_{3}^{T}(s,t)ds,\dots, \int_{-d_{pM}}^{-p\bar{w}} \mathscr{L}_{3}^{T}(s,t)ds,\dots, \int_{-d_{NM}}^{-N\bar{w}} \mathscr{L}_{3}^{T}(s,t)ds]^{T}, \quad \mathscr{L}_{i}(s,t) = \mathbb{L}^{i}(s)x(t+s).$

Construct the following Lyapunov function:

$$V(t) = V_1(t) + V_2(t) + V_3(t) + V_4(t)$$
(15)

where

$$V_{1}(t) = \zeta^{T}(t)P\zeta(t)$$

$$V_{2}(t) = \sum_{p=1}^{N} \int_{-d_{(p-1)M}}^{-(p-1)\bar{w}} x^{T}(t+s) [\mathcal{T}_{2p} + sQ_{1p}]x(t+s)ds$$

$$V_{3}(t) = \sum_{p=1}^{N} \int_{-p\bar{w}}^{-(p-1)\bar{w}} x^{T}(t+s) [\mathcal{T}_{3p} + sQ_{2p}]x(t+s)ds$$

$$V_{4}(t) = \sum_{p=1}^{N} \int_{-d_{pM}}^{-p\bar{w}} x^{T}(t+s[\mathcal{T}_{4p} + sQ_{3p}]x(t+s)ds$$

with $\mathcal{T}_{2p} = R_{1p} + d_{(p-1)M}Q_{1p}$, $\mathcal{T}_{3p} = R_{2p} + p\bar{w}Q_{2p}$, and $\mathcal{T}_{4p} = R_{3p} + d_{pM}Q_{3p}$.

Taking the derivative of V(t) along (12) results in

$$\dot{V}(t) = 2\zeta^{T}(t)P\dot{\zeta}(t) + \sum_{s=2}^{4}\sum_{p=1}^{N}\dot{V}_{sp}(t)$$
(16)

where

$$\begin{split} \dot{V}_{2p}(t) &= x^{T}(t - (p - 1)\bar{w})\hat{\mathcal{T}}_{2p}x(t - (p - 1)\bar{w}) \\ &- x^{T}(t - d_{(p - 1)M})R_{1p}x(t - d_{(p - 1)M}) \\ &- \int_{-d_{(p - 1)M}}^{-(p - 1)\bar{w}} x^{T}(t + s)Q_{1p}x(t + s)ds \\ \dot{V}_{3p}(t) &= x^{T}(t - (p - 1)\bar{w})\hat{\mathcal{T}}_{3p}x(t - (p - 1)\bar{w}) \\ &- x^{T}(t - p\bar{w})R_{2p}x(t - p\bar{w}) \\ &- \int_{-p\bar{w}}^{-(p - 1)\bar{w}} x^{T}(t + s)Q_{2p}x(t + s)ds \end{split}$$

$$\dot{V}_{4p}(t) = x^{T}(t - p\bar{w})\hat{\mathcal{T}}_{4p}x(t - p\bar{w}) - x^{T}(t - d_{pM})R_{3p}x(t - d_{pM}) - \int_{-d_{pM}}^{-p\bar{w}} x^{T}(t + s)Q_{3p}x(t + s)ds.$$

According to Lemma 1

$$-\sum_{p=1}^{N} \int_{-d_{(p-1)M}}^{-(p-1)\bar{w}} x^{T}(t+s)Q_{1(p-1)}x(t+s)ds$$

$$\leq [\mathbf{K}\Omega_{1}(t)]^{T}(W_{\nu} \otimes \mathfrak{Q}_{1})[\mathbf{K}\Omega_{1}(t)]$$

$$-\sum_{p=1}^{N} \int_{-p\bar{w}}^{-(p-1)\bar{w}} x^{T}(t+s)Q_{2p}x(t+s)ds$$

$$\leq [\mathscr{L}^{2}(t)]^{T}(W_{\nu} \otimes \mathfrak{Q}_{2})[\mathscr{L}^{2}(t)]$$

$$-\sum_{p=1}^{N} \int_{-d_{pM}}^{-p\bar{w}} x^{T}(t+s)Q_{3p}x(t+s)ds$$

$$\leq [\mathbf{K}\Omega_{3}(t)]^{T}(W_{\nu} \otimes \mathfrak{Q}_{3})[\mathbf{K}\Omega_{3}(t)]$$

where

$$\begin{split} \Omega_1(t) &= \begin{bmatrix} \Omega_1^{1T}(t) & \cdots & \Omega_1^{pT}(t) & \cdots & \Omega_1^{NT}(t) \end{bmatrix}^T \\ \Omega_3(t) &= \begin{bmatrix} \Omega_3^{1T}(t) & \cdots & \Omega_3^{pT}(t) & \cdots & \Omega_3^{NT}(t) \end{bmatrix}^T \\ \Omega_1^p(t) &= \begin{bmatrix} \Omega_{1,1}^p(t) \\ \Omega_{1,2}^p(t) \end{bmatrix}, \ \Omega_3^p(t) &= \begin{bmatrix} \Omega_{3,1}^p(t) \\ \Omega_{3,2}^p(t) \end{bmatrix} \\ \Omega_{1,2}^p(t) &= \int_{-d_{p-1}(t)}^{-d_{p-1}(t)} \mathbb{L}^1(s)x(t+s)ds \\ \Omega_{3,2}^p(t) &= \int_{-d_{pM}}^{-d_{p}(t)} \mathbb{L}^3(s)x(t+s)ds. \end{split}$$

We recall the triggering condition in (6)

$$-\varepsilon^{T}(t)\Lambda\varepsilon(t) + \theta\bar{x}^{T}(i_{k}h)\Lambda\bar{x}(i_{k}h) \ge 0$$
(17)

which is equivalent to

$$\begin{bmatrix} \varepsilon(t) \\ \bar{x}(i_kh) \end{bmatrix}^T \begin{bmatrix} -\Lambda & 0 \\ 0 & \theta\Lambda \end{bmatrix} \begin{bmatrix} \varepsilon(t) \\ \bar{x}(i_kh) \end{bmatrix} \ge 0.$$
(18)

According to the bound and differentiation property of $L_i(s)$

$$\dot{\mathcal{L}}_{1}^{p}(t) = \mathbf{J}x(t - (p - 1)\bar{w}) - \hat{\mathbf{J}}x(t - d_{(p-1)M}) - \frac{\Pi_{\nu}}{\eta_{M}} \left(\Omega_{1,1}^{p}(t) + \Omega_{1,2}^{p}(t)\right)$$
(19)

$$\dot{\mathcal{L}}_{2}^{p}(t) = \mathbf{J}x(t - (p - 1)\bar{w}) - \hat{\mathbf{J}}x(t - p\bar{w}) - \frac{\Pi_{\nu}}{\bar{w}}\Omega_{2}^{p}(t)$$
(20)
$$\dot{\mathcal{L}}_{3}^{p}(t) = \mathbf{J}x(t - p\bar{w}) - \hat{\mathbf{J}}x(t - d_{pM})$$

$$\int_{3}^{p} f(t) = \mathbf{J} x(t - p\bar{w}) - \mathbf{J} x(t - d_{pM}) - \frac{\Pi_{\nu}}{\eta_{M}} \Big(\Omega_{3,1}^{p}(t) + \Omega_{3,2}^{p}(t) \Big).$$
 (21)

By defining $\vartheta(t) = [\dot{x}^T(t), x^T(t), x^T(t) - \bar{w}], \dots, x^T(t - N\bar{w}), x^T(t - d_{0M}), \dots, x^T(t - d_{NM}), \Omega_1^T(t), \Omega_2^T(t), \Omega_3^T(t)\varepsilon^T(t), d^T(t), z^T(t)]^T$, we obtain

$$\zeta(t) = \mathcal{M}\vartheta(t), \ \zeta(t) = \mathcal{H}\vartheta(t).$$
(22)

From (12), one has

$$\vartheta^{T}(t)\mathbf{He}(\mathcal{GF})\vartheta(t) = 0$$
(23)
where $\mathcal{G} = \mathbb{I}_{1}^{T}G + \alpha \mathbb{I}_{2}^{T}G.$

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To ensure H_{∞} stability of system (12), the following condition is needed:

$$\begin{split} \dot{V}(t) + z^{T}(t)z(t) &- \gamma^{2}d^{T}(t)d(t) \leq \vartheta^{T}(t)\mathbf{He}\left(\mathcal{M}^{T}P\mathcal{H}\right)\vartheta(t) \\ &+ \sum_{p=1}^{N} \left[\mathbf{Sy}\left(\hat{\mathcal{T}}_{2p}, \mathbb{I}_{1+p}\vartheta(t)\right) - \mathbf{Sy}\left(R_{1p}, \mathbb{I}_{2+p+N}\vartheta(t)\right)\right] \\ &- \mathbf{Sy}\left(W_{\nu}\otimes\mathfrak{Q}_{1}, \mathbf{K}\mathbb{E}_{1,N}\vartheta(t)\right) \\ &+ \sum_{p=1}^{N} \left[\mathbf{Sy}\left(\hat{\mathcal{T}}_{3p}, \mathbb{I}_{1+p}\vartheta(t)\right) - \mathbf{Sy}\left(R_{2p}, \mathbb{I}_{2+p}\vartheta(t)\right)\right] \\ &- \mathbf{Sy}(W_{\nu}\otimes\mathfrak{Q}_{2}, \mathbb{E}_{2,N}\vartheta(t)) \\ &+ \sum_{p=1}^{N} \left[\mathbf{Sy}\left(\hat{\mathcal{T}}_{4p}, \mathbb{I}_{2+p}\vartheta(t)\right) - \mathbf{Sy}\left(R_{3p}, \mathbb{I}_{3+p+N}\vartheta(t)\right)\right] \\ &- \mathbf{Sy}(W_{\nu}\otimes\mathfrak{Q}_{3}, \mathbf{K}\mathbb{E}_{3,N}\vartheta(t)) - 0.2785\mu_{0} \\ &+ \mathbf{Sy}\left(\left[\begin{matrix} -\Lambda & 0\\ 0 & \theta\Lambda\end{matrix}\right], \left[\begin{matrix} \mathbb{I}_{\varepsilon}\\ \mathbb{I}_{\bar{x}}\\ \end{matrix}\right]\vartheta(t)\right) \\ &- \gamma^{2}\mathbf{Sy}(I_{q}, \mathbb{I}_{d}\vartheta(t)) - \mathbf{Sy}(I_{r}, \mathbb{I}_{z}\vartheta(t)) \\ &+ \vartheta^{T}(t)\mathbf{He}\left(\mathbb{I}_{z}^{T}C\mathbb{I}_{2}\right)\vartheta(t) + \mathbf{Sy}(\mathbf{He}(\mathcal{GF}), \vartheta(t)) < 0 \end{split}$$

which is guaranteed by (14). Thus, the proof is completed.

Remark 10: In this study, we focus on designing an eventtriggered control method with SWI. Moreover, $V_3(t)$ and $V_4(t)$ in (15) help introduce SWI by using the properties of Legendre polynomials. In addition, *P* in $V_1(t)$ does not need to be positive definite; thus, the results are less conservative.

Theorem 2: For the scalars \bar{w} , α , θ , and the prespecified H_{∞} attenuation level γ , the system (1) with the controller in (3) and the SWI-based ETM in (6) is asymptotically stable if there exist symmetric matrices \tilde{P} , $\tilde{R}_{1p} > 0$, $\tilde{R}_{2p} > 0$, $\tilde{R}_{3p} > 0$, $\tilde{Q}_{1p} > 0$, $\tilde{Q}_{2p} > 0$, $\tilde{Q}_{3p} > 0$, $\tilde{Y}_{1p} > 0$, $\tilde{Y}_{3p} > 0$, $\tilde{\Lambda} > 0$, $\tilde{Q}_{1(p-1)} = \begin{bmatrix} \tilde{Q}_{1p} & \tilde{Y}_{1p} \\ \tilde{Y}_{1p} & \tilde{Q}_{1p} \end{bmatrix} > 0$, and $\tilde{Q}_{3p} = \begin{bmatrix} \tilde{Q}_{3p} & \tilde{Y}_{3p} \\ \tilde{Y}_{3p} & \tilde{Q}_{3p} \end{bmatrix} > 0$ with $p = 1, \dots, N$ and matrices X and Y such that

$$\mathscr{P} > 0, \text{ and } \Theta < 0$$
 (24)

where

$$\begin{split} \tilde{\mathscr{P}} &= \tilde{P} + \operatorname{diag} \left\{ 0, \tilde{\mathfrak{Q}}_{1}, \tilde{\mathfrak{Q}}_{2}, \tilde{\mathfrak{Q}}_{3} \right\} \\ \tilde{\Theta} &= \operatorname{He}(\mathcal{M}^{T} \tilde{P} \mathcal{H}) \\ &+ \sum_{p=1}^{N} \left[\operatorname{Sy}(\tilde{\mathcal{T}}_{2p}, \mathbb{I}_{1+p}) - \operatorname{Sy}(\tilde{R}_{1p}, \mathbb{I}_{2+p+N}) \right] \\ &- \operatorname{Sy}(W_{\nu} \otimes \tilde{\mathfrak{Q}}_{1}, \mathbf{K} \mathbb{I}_{1,N}) \\ &+ \sum_{p=1}^{N} \left[\operatorname{Sy}(\tilde{\mathcal{T}}_{3p}, \mathbb{I}_{1+p}) - \operatorname{Sy}(\tilde{R}_{2p}, \mathbb{I}_{2+p}) \right] \\ &+ \sum_{p=1}^{N} \left[\operatorname{Sy}(\tilde{\mathcal{T}}_{4p}, \mathbb{I}_{2+p}) - \operatorname{Sy}(\tilde{R}_{3p}, \mathbb{I}_{3+p+N}) \right] \\ &- \operatorname{Sy}(W_{\nu} \otimes \tilde{\mathfrak{Q}}_{2}, \mathbb{I}_{2,N}) - \operatorname{Sy}(W_{\nu} \otimes \tilde{\mathfrak{Q}}_{3}, \mathbf{K} \mathbb{I}_{3,N}) \\ &+ \operatorname{Sy}\left(\begin{bmatrix} -\tilde{\Lambda} & 0 \\ 0 & \theta \tilde{\Lambda} \end{bmatrix}, \begin{bmatrix} \mathbb{I}_{\varepsilon} \\ \mathbb{I}_{\bar{x}} \end{bmatrix} \right) - \gamma^{2} \operatorname{Sy}(I_{q}, \mathbb{I}_{d}) - \operatorname{Sy}(I_{r}, \mathbb{I}_{z}) \\ &+ \operatorname{He}(\mathbb{I}_{z}^{T} C X \mathbb{I}_{2}) + \operatorname{He}(\tilde{\mathcal{G}} \tilde{\mathcal{F}}) \end{split}$$

$$\begin{aligned} \mathcal{F} &= -X\mathbb{I}_1 + AX\mathbb{I}_2 + BY\mathbb{I}_{\check{x}} - BY\mathbb{I}_{\varepsilon} + E\mathbb{I}_d \\ &+ BY\sum_{p=1}^N \frac{\mu_p}{\bar{w}} \Big[\mathbb{I}_2^p + \mathbb{I}_{3,1}^p - \mathbb{I}_{1,1}^p \Big]. \end{aligned}$$

Then, the weight matrix of the SWI-based ETM and the controller gain can be solved with $\Lambda = X^{-1} \tilde{\Lambda} X^{-1}$ and $K = YX^{-1}$, respectively.

Proof: Define

$$\begin{split} X &= G^{-1}, \ \tilde{P} = \left(I_{(1+5(\varrho+1))n} \otimes X \right) P \left(I_{(1+5(\varrho+1))n} \otimes X \right) \\ \tilde{\mathcal{T}}_{sp} &= X \hat{\mathcal{T}}_{sp} X, \ \tilde{R}_{(s-1)p} = X R_{(s-1)p} X \\ p &= 1, 2, \dots, N, \ s = 2, 3, 4 \\ \tilde{\mathfrak{Q}}_1 &= \mathcal{X} \mathfrak{Q}_1 \mathcal{X}, \ \tilde{\mathfrak{Q}}_2 &= \mathcal{X}_2 \mathfrak{Q}_2 \mathcal{X}_2, \ \tilde{\mathfrak{Q}}_3 = \mathcal{X} \mathfrak{Q}_3 \mathcal{X} \\ \mathcal{X} &= I_{(N(\varrho+1))2n} \otimes X, \ \mathcal{X}_2 = I_{(N(\varrho+1))n} \otimes X \\ \tilde{Y}_{1p} &= X Y_{1p} X, \ \tilde{Y}_{3p} = X Y_{3p} X, \ \tilde{\Lambda} = X \Lambda X. \end{split}$$

Pre- and post-multiplying (25) by $\mathscr{X} =$ diag{ $X, X, X_1, X_2, X, X, I, I$ }, $X_1 =$ diag{ X, \ldots, X },

$$X_2 = \text{diag}\{\underbrace{X, \dots, X}_{5N(\nu+1)}\}$$
 and its transpose yields

$$\tilde{\Theta} < 0$$
 (25)

which is ensured by (24). Thus, the proof is complete.

IV. NUMERICAL EXAMPLE

This section presents a simulation example to validate the proposed SWI-based event-triggered control strategy.

Example 1: Consider the system (1) with the following parameters:

$$A = \begin{bmatrix} 0 & 1\\ 0.5 & -3 \end{bmatrix}, B = \begin{bmatrix} 0\\ 2 \end{bmatrix}, E = \begin{bmatrix} 5\\ 2 \end{bmatrix}, C = \begin{bmatrix} 2 & 1.5 \end{bmatrix}.$$

Let the sampling period be h = 0.005 s and the possible maximum transmission delay be $\bar{d}_l = 0.05$ s, then $\eta_M = \bar{d}_l + h = 0.055$ s.

The scale of the SHW is w = 0.045 s. Three parts (N = 3) with the weights $\mu_1 = 0.6$, $\mu_2 = 0.3$, and $\mu_3 = 0.1$ are segmented. For $\gamma = 1$, $\theta = 0.05$, and $\alpha = 150$, we obtain the controller gain in (3) and the triggering parameter of the ETM in (5) from Theorem 2 with the MATLAB Toolbox:

$$K = \begin{bmatrix} -1.0309 & -0.6962 \end{bmatrix}, \quad \Lambda = \begin{bmatrix} 0.3428 & 0.2315 \\ 0.2315 & 0.1564 \end{bmatrix}.$$
(26)

The initial condition is $x(0) = [2 - 1]^T$; and the disturbance is $d(t) = r(t)e^{-0.5t}$ for 0 < t < 6 s and zero for t > 6 s, where r(t) denotes a stochastic variable satisfying |r(t)| < 10.

For the previously presented parameters, we obtain the simulation results shown in Fig. 2; evidently, the system can successfully be stabilized under the proposed communication and control scheme.

To show the influence of the segmented weight on the system performance and the amount of transmitted data, we set N = 1; that is, the state in the whole SHW has the weight $\mu = 1$. The other parameters are identical to those for the



Fig. 2. State responses under the SWI-based ETM with N = 3.



Fig. 3. State responses under SWI-based ETM with N = 1.

case with N = 3. Similarly, we obtain the parameters of the controller in (3) and the SWI-based ETM in (5) via Theorem 2

$$K = \begin{bmatrix} -2.1088 & -1.5404 \end{bmatrix}, \quad \Lambda = \begin{bmatrix} 2.6819 & 1.9590 \\ 1.9590 & 1.4311 \end{bmatrix}.$$
(27)

Fig. 3 presents the state responses for these parameters. According to Figs. 2 and 3, one can know that the control strategy and ETM with SWI, where N = 1 and N = 3, can result in good control performance.

To investigate the amount of transmitted data under the traditional ETM, the SWI-based ETM with (N = 1), and our proposed SWI-based ETM (N = 3), the release instants and their corresponding release intervals are presented in Fig. 4. Evidently, our proposed SWI-based ETM leads to fewer transmitted data. Table I presents the detailed amount of transmitted data; only 14.2% of the sampling packets are transmitted over the network if the proposed SWI-based ETM with N = 3is adopted, 16.5% is transmitted for N = 1; by contrast, the data-release rate increases to 20.3% for traditional ETM. Therefore, our proposed SWI-based ETM can significantly save network communication resources while maintaining the control performance at a certain level.



Fig. 4. Releasing instants under the traditional ETM in [24] and SWI-based ETMs with N = 1 and 3.

TABLE I Amount of Data Transmission (\mathcal{N}) Under Different Communication Mechanisms

Communication mechanism	\mathcal{N}
Traditional ETM in [24]	406
SWI-based ETM with $N = 1$	330
SWI-based ETM with $N = 3$	284

TABLE II Amount of Transmitted Data (\mathcal{N}) of Different Communication Mechanisms

Communication mechanism	\mathcal{N}
Traditional ETM in [24]	560
SWI-based ETM with $N = 1$	493
SWI-based ETM with $N = 3$	388

Example 2: In this example, we consider the decoupled linearized dynamics of a practical F-18 aircraft studied in [37]

$$\begin{bmatrix} \dot{\alpha}(t) \\ \dot{q}(t) \end{bmatrix} = \begin{bmatrix} -1.175 & 0.9871 \\ -8.45 & -0.8776 \end{bmatrix} \begin{bmatrix} \alpha(t) \\ q(t) \end{bmatrix} \\ + \begin{bmatrix} -0.194 & -0.03593 \\ -19.29 & -3.803 \end{bmatrix} \begin{bmatrix} \delta_E(t) \\ \delta_{PTV}(t) \end{bmatrix} + \begin{bmatrix} 1 \\ 4 \end{bmatrix} d(t)$$

where $\alpha(t)$ and q(t) are the attack angle and pitch rate; they are chosen as the state. The control inputs are the symmetric elevator position $\delta_E(t)$ and symmetric pitch thrust velocity nozzle position $\delta_{PTV}(t)$.

For $\gamma = 1$, by solving the conditions in Theorem 2 with the design parameters in Example 1, we obtain the controller gains and triggering matrices for N = 1 and N = 3

$$K = \begin{bmatrix} 89.9648 & 56.0419 \\ -456.3525 & -284.1305 \end{bmatrix}, \ \Lambda = \begin{bmatrix} 0.2541 & 0.2262 \\ 0.2262 & 0.3030 \end{bmatrix}$$
for $N = 1$ and
$$K = \begin{bmatrix} 33.1511 & -1.5255 \\ -168.1628 & 7.8409 \end{bmatrix}, \ \Lambda = \begin{bmatrix} 0.0654 & -0.0021 \\ -0.0021 & 0.0530 \end{bmatrix},$$
for $N = 3$.



Fig. 5. State responses of the F-18 aircraft under the SWI-based ETM with N = 1.



Fig. 6. Release instants and release intervals under SWI-based ETM with N = 1.

The initial condition is assumed to be $x(0) = [1 - 2]^{\top}$, and the disturbance is $d(t) = r(t)e^{-0.3t}$ for 0 < t < 8 s, and 0 for t > 8 s, where r(t) is a stochastic variable satisfying |r(t)| < 5.

The state responses and triggering instants for N = 1 and N = 3 are presented in Figs. 5–8. Moreover, the amount of transmitted data under the traditional ETM, SWI-based ETM for N = 1, and proposed SWI-based ETM for N = 3 are presented in Table II. From these figures and the table, we can get similar conclusions from Example 1 that the proposed SWI-based ETM helps reduce redundant triggering events and saves more network resources, in particular for systems subject to random disturbances.

V. CONCLUSION

An SWI-based event-triggered control method forNCSs was developed. The sampler samples SWI in the SWH from the plant rather than the current state or current measurement output. This processing method can reduce the loss of information caused by direct periodic sampling. Furthermore, using the historical averaged information as the decision variable instead



Fig. 7. State responses of the F-18 aircraft under the SWI-based ETM with N = 3.



Fig. 8. Release instants and release intervals under SWI-based ETM with N = 3.

of the information of certain instants is more reasonable, in particular, for a system with uncertain or stochastic disturbances. In addition, the Zeno phenomenon is prevented. The simulation example shows that this proposed method fully exploit historical information and effectively balance the system performance and use of network resources. In the future, the proposed SWI-based ETM can be extended to nonlinear systems by combining the methods in [38], [39], and [40] to address practical problems.

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